
Negative resistance oscillators

Terminology:

- load matching network (or resonant matching network) determines the frequency of oscillation
- terminating network is used to provide proper matching

One port negative resistance oscillators (fig. 5.2.1)

Negative resistance device represented by amplitude and frequency dependent impedance $Z_{IN}(V, \omega) = R_{IN}(V, \omega) + X_{IN}(V, \omega)$.
 $R_{IN}(V, \omega) < 0$ for some V and some ω .

Oscillator constructed by connecting the neg. resistance device to a passive load impedance $Z_L = R_L + X_L$



Recall stability conditions of two-ports. To make devices unconditionally stable we used resistive loading. Just because device is not unconditionally stable does not mean it is actually going to oscillate — total resistance in the loop must be negative.

By analogy: 1-port is stable if $\text{Re}[Z_{IN}(V, \omega) + Z_L(\omega)] > 0$.

For network to actually oscillate the requirement is:

$$\Gamma_{IN}(V, \omega)\Gamma_L(\omega) = 1 \quad (1)$$

Explain in terms of reflected/incident waves. $|\Gamma| > 1$ means that there is an amplification of reflected signal.

Eq. 1 can be broken into two parts:

$$R_{IN}(V, \omega) + R_L = 0 \quad \text{and} \quad X_{IN}(V, \omega) + X_L(\omega) = 0 \quad (2)$$



Instability vs. oscillation: instability results in an uncontrolled increase of voltage and current and it has no steady state. Oscillation is a “stable” state (steady state), i.e. the amplitudes do not grow uncontrollably.

Define device as unstable over some freq. range (ω_1, ω_2) if $R_{IN} < 0$ on that range.

One port network is unstable for some ω_0 on (ω_1, ω_2) if the net resistance of the network is negative, i.e. $|R_{IN}(V, \omega)| > R_L$. Any excitation or noise can initiate such network to oscillate with ω_0 for which the net reactance of the network is equal to zero, i.e.

$$X_L(\omega_0) = X_{IN}(V, \omega_0)$$



At ω_0 a growing sinusoidal current will flow through the circuit. Growth continues for as long as the resistance is negative ($|\Gamma| > 1$). This cannot go on forever and some non-linearity must bring about change in $|R_{IN}|$ so that when voltage V across it reaches some level ($V = V_0$) the net resistance reaches zero value $R_{IN}(V_0, \omega_0) + R_L = 0$.

Problem: oscillation frequency is not stable. It is determined from the condition on reactance $X_{IN}(V, \omega)$ which changes as V increases. For stable oscillation an additional condition is needed. Kurokawa came up with it for $Z_{IN}(V, \omega)$ that is essentially constant in ω around ω_0 :

$$\left. \frac{\partial R_{IN}(V, \omega)}{\partial V} \right|_{V=V_0} \quad \left. \frac{\partial X_L(\omega)}{\partial \omega} \right|_{\omega=\omega_0} \quad - \quad \left. \frac{\partial X_{IN}(V, \omega)}{\partial V} \right|_{V=V_0} \quad \left. \frac{\partial R_L(\omega)}{\partial \omega} \right|_{\omega=\omega_0} > 0 \quad (3)$$



3 requirements for stable oscillations. Since $\partial R_L(\omega)/\partial\omega = 0$, eq. 3 can be simplified.

Example 5.2.1. Device is modeled as a parallel combination of G and C , $G(V) = G_M(1 - V/V_m)$. Find a load circuit (Z_L) to provide oscillation at ω_0 and calculate output power.

- $Z_{in}(V, \omega) = R_{in} + X_{in} = -\frac{G(V)}{G^2(V) + \omega^2 C^2} + \frac{-\omega C}{G^2(V) + \omega^2 C^2}$ (4)

- 1st condition:

$$R_L = \frac{G(V)}{(G^2(V) + \omega^2 C^2)} \Big|_{\omega=\omega_0, V=V_0} \quad (5)$$

(note: this does not mean R_L is freq. dependent!)



- for X we have

$$X_L(\omega) = \frac{\omega C'}{(G^2(V) + \omega^2 C'^2)} \Big|_{\omega=\omega_0, V=V_0} \quad (6)$$

- 3rd condition:

$$\frac{\partial R_{IN}}{\partial V} \Big|_{V=V_0} \frac{\partial X_L}{\partial \omega} \Big|_{\omega=\omega_0} > 0 \quad (7)$$

